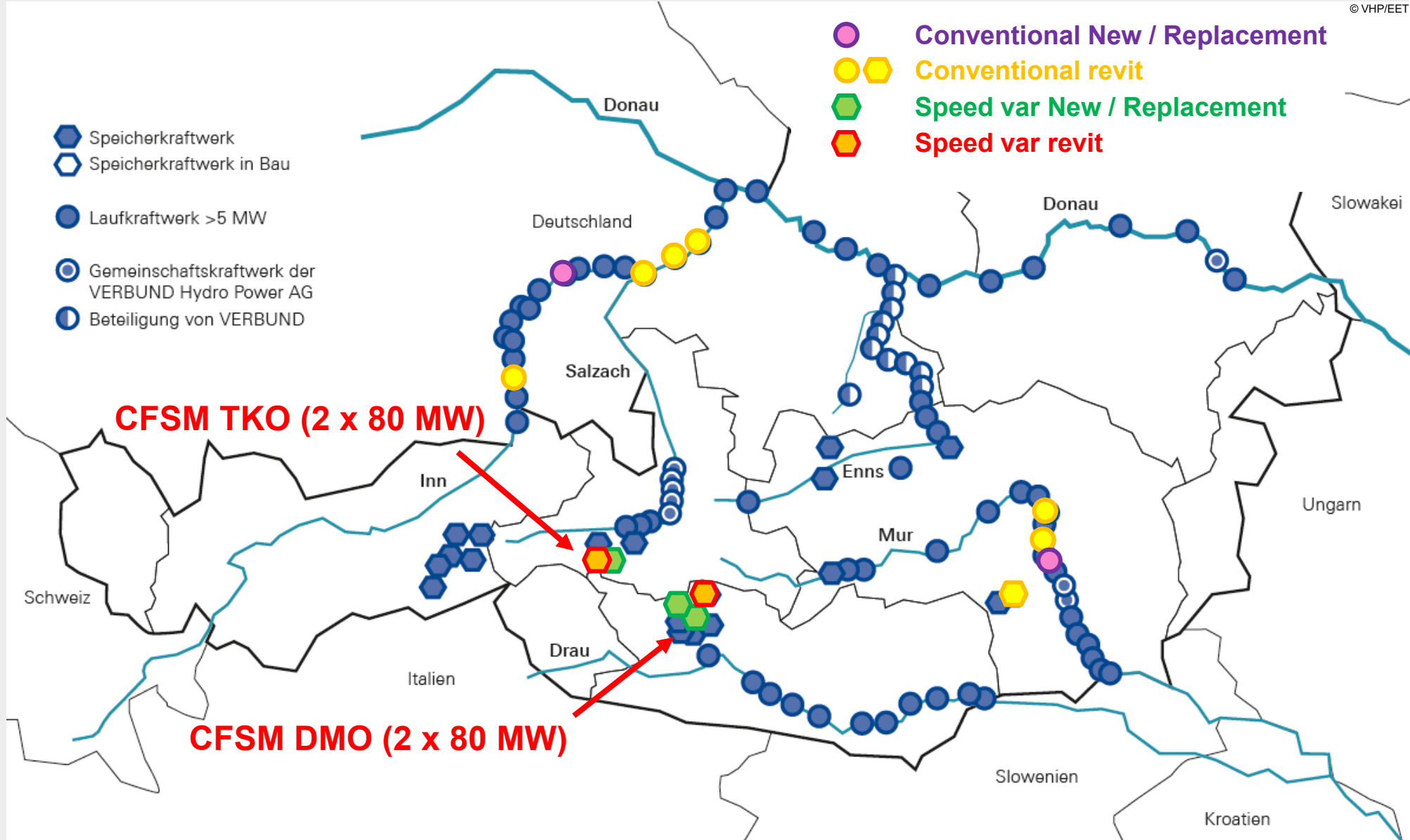


Verbund Hydro Power

Stefan Polster – stefan.polster@verbund.com
26.06.2023



Verbund power plants and recent projects



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Commissioned Projects DMO and TKO

Polster
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Overhaul Project Malta Oberstufe I

Original Pumped Storage Design

In operation since 1977

- 2x 60MW synchronous machines
 - Pole-changing motor-generator
 - (375 - 500 rpm)

Isogyr hydraulic system

- Separated pump and turbine

New Design

After Overhaul 2022
«Efficiency Increase»

- 2x 80MW Converter Fed Synchronous Machine
 - Variable speed operation (240...575 rpm)
 - Modular Multilevel Converter

New Motor-Generator

New machine transformer

New reversible pump-turbine

- Reuse of existing structures



Malta Oberstufe Overhaul Project Variable Speed Operation with MMC Full Converter
Vienna Hydro 2022

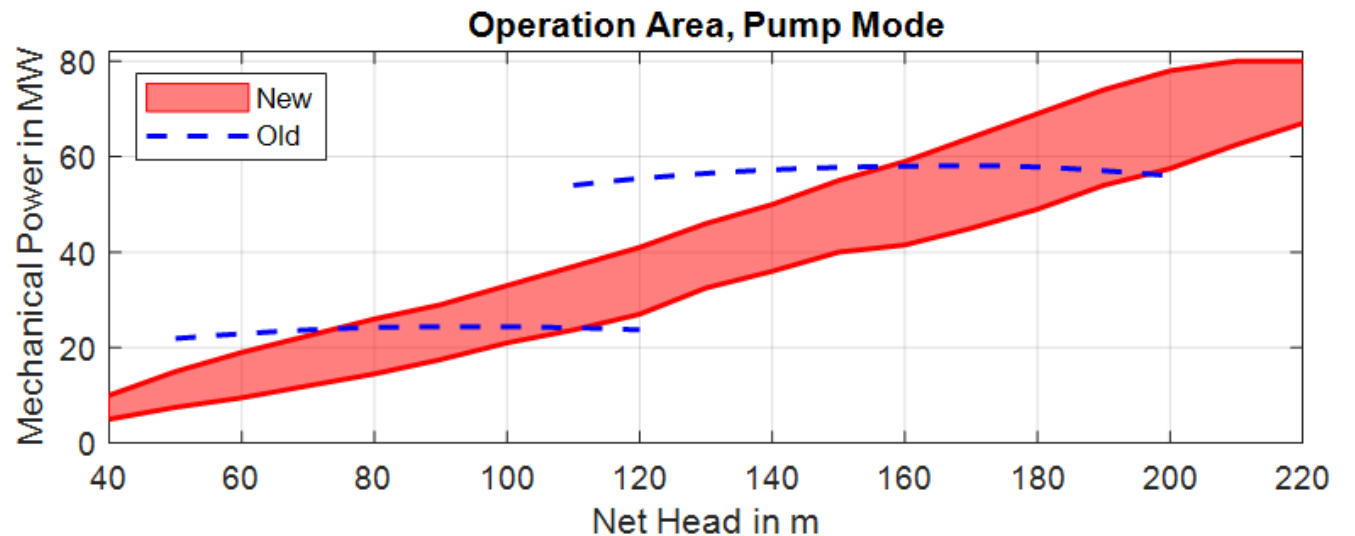
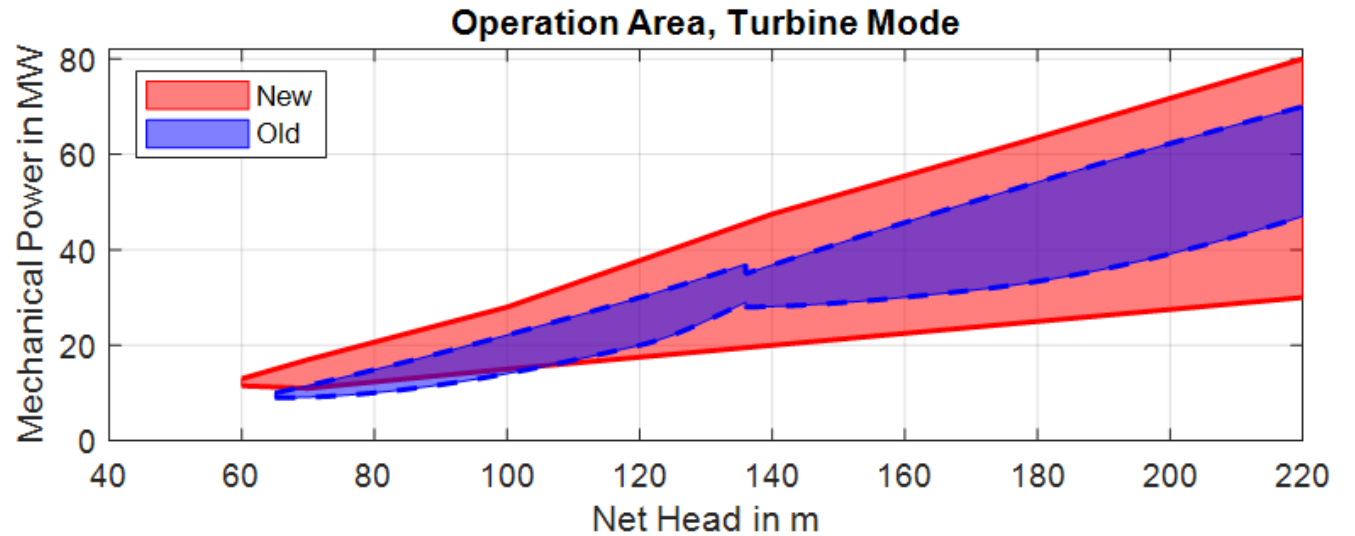
Overhaul Project Malta Oberstufe IV

Turbine Mode

- Extended net head
- Wider power range window
- Efficiency improvement around 9% averaged in the operation area

Pump Mode

- Active power control
- Extended head range 40 to 220 m
- Optimized operation for each head
- Efficiency improvement between 15 to 22 %



Malta Oberstufe Overhaul Project Variable Speed Operation With MMC Full Converter
Vienna Hydro 2022

CIGRE NGN 26.06.2023

Overhaul Project Kaprun Oberstufe I

Original Pumped Storage Design

In operation since 1956

- 2x 65 MW synchronous machine
 - 500 rpm
 - Head range (288 m – 446 m)
 - 56 MW Francis turbines
 - 65 MW radial pump

New Design

After Overhaul
2020 - 2022
«Efficiency Increase»

- 2x 80MW Converter Fed Synchronous Machine
 - Variable speed operation (400...730 rpm)
 - Voltage Source Inverter
- New Motor-Generator
- New machine transformer
- New reversible pump-turbine
 - Reuse of existing structures



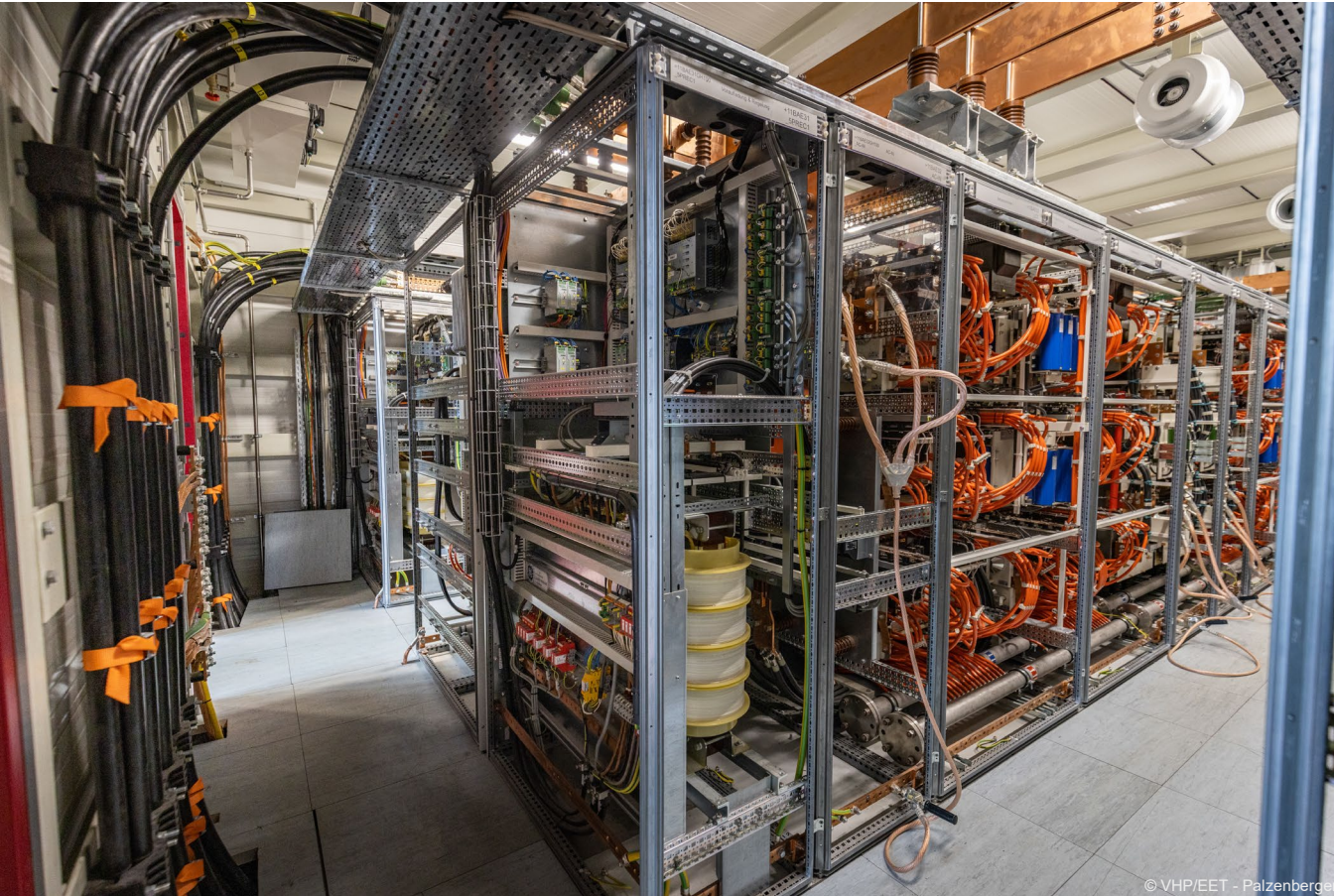
Overhaul Project Kaprun Oberstufe III



Overhaul Project Kaprun Oberstufe IV



Overhaul Project Kaprun Oberstufe V



Technical aspects and operation experience

Polster
26.06.2023



Converter Technologies

Voltage Source Converter

TKO – 3-level converter

Output voltage 3 conditions

- Aggressive voltage form
- Current ripple

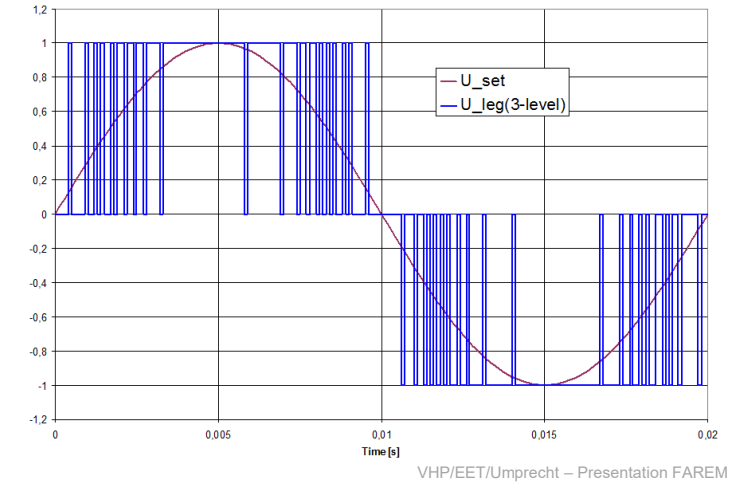
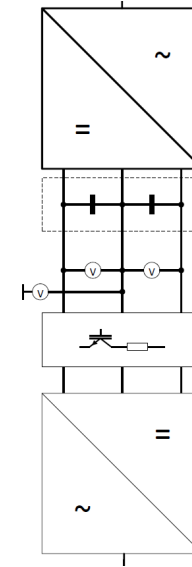
Frequency range

- 0 to 51 Hz (higher with output filter)

Multi-winding transformer necessary

Redundancy on converter level

- Failed output switch takes out converter



VHP/EET/Umprecht – Presentation FAREM

Direct Converter

DMO - MMC

Output voltage smoother

- Depends on number of serial cells

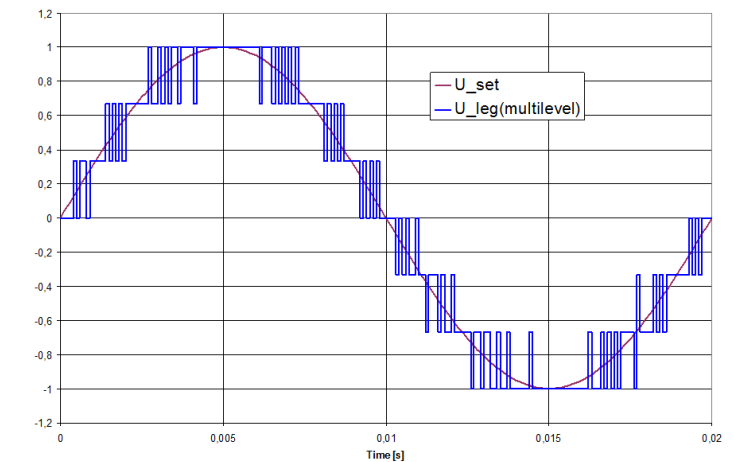
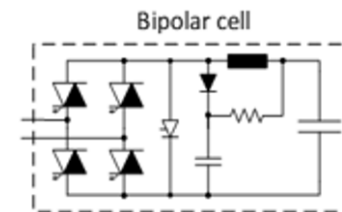
Frequency range

- 0 to ~42 Hz

Possible with two-winding transformer

Redundancy on cell level

- Continued operation with failed cell



VHP/EET/Umprecht – Presentation FAREM

Design Considerations – Power Train

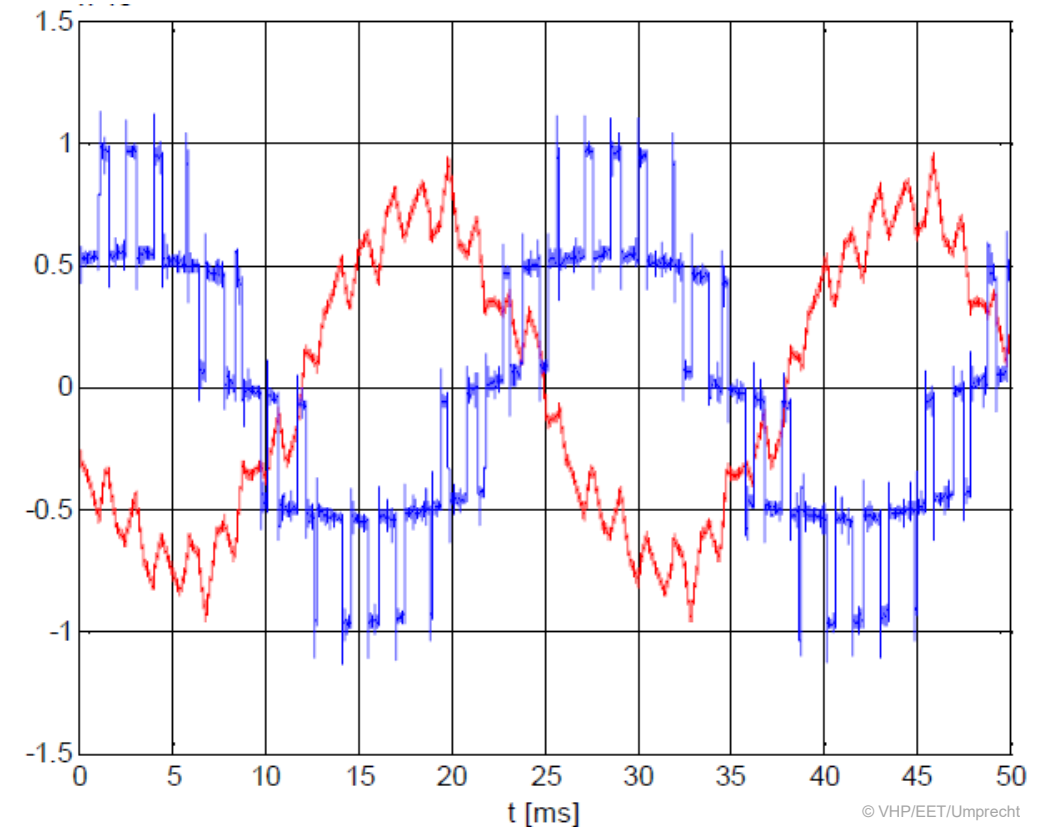
Electrical

- Stator voltage form (THD factor, high du/dt)
- Higher insulation stress and particle discharge level
 - Capacitive coupling
 - Heating of potential grading
 - Shaft voltage

- Stator current form (THD factor, ripple)
- Additional losses and changed loss distribution
 - Pulsing moments

Mechanical

- Design for speed area
- Eigenfrequencies + Resonances
 - Torsional oscillations
 - Noise emission
 - Vibrations



Operation flexibility

Technology benefit CFSM

Increased area of operation

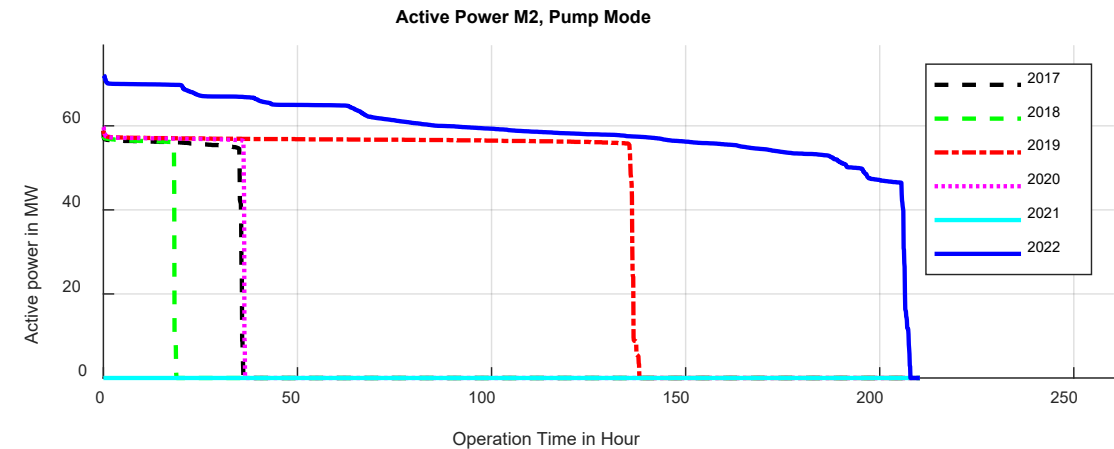
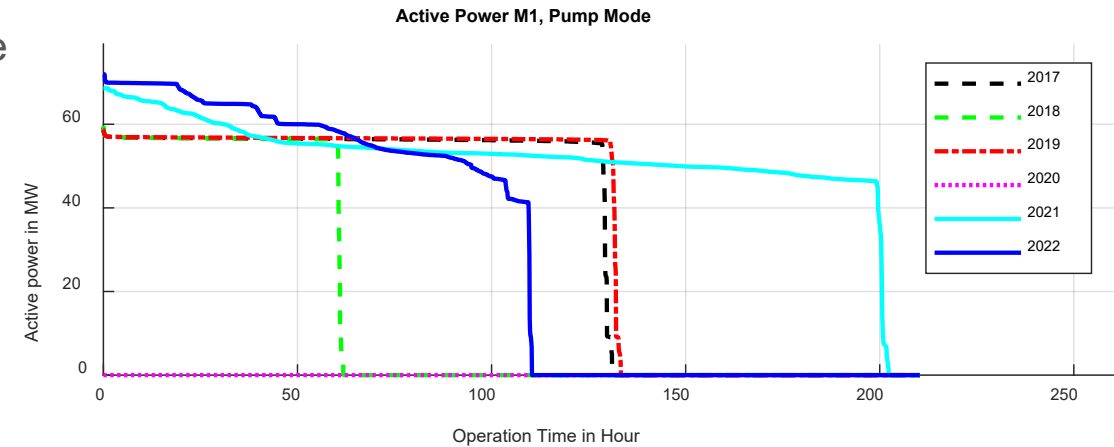
Active power control operation in pump mode

- Provision of grid frequency support
- Participation to primary control possible
- Higher flexibility for unit commitment

Impact on pump operation

Utilization of variable power

- Increased operational hours
- Extended operation time per start



Malta Oberstufe Overhaul Project Variable Speed Operation With MMC Full Converter
Vienna Hydro 2022

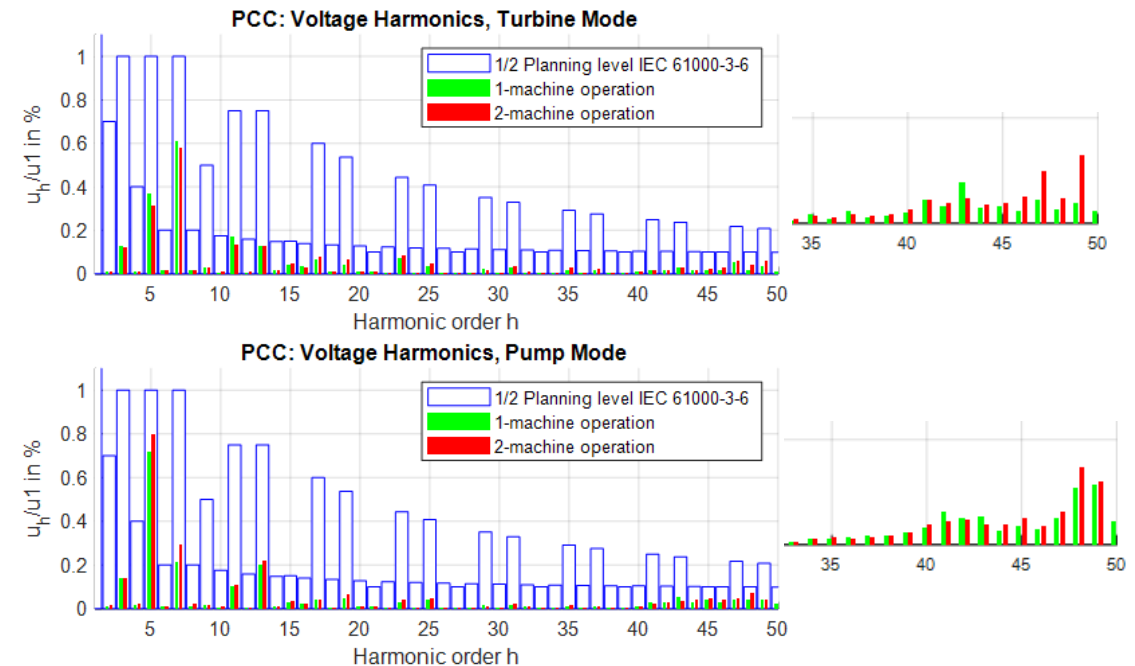
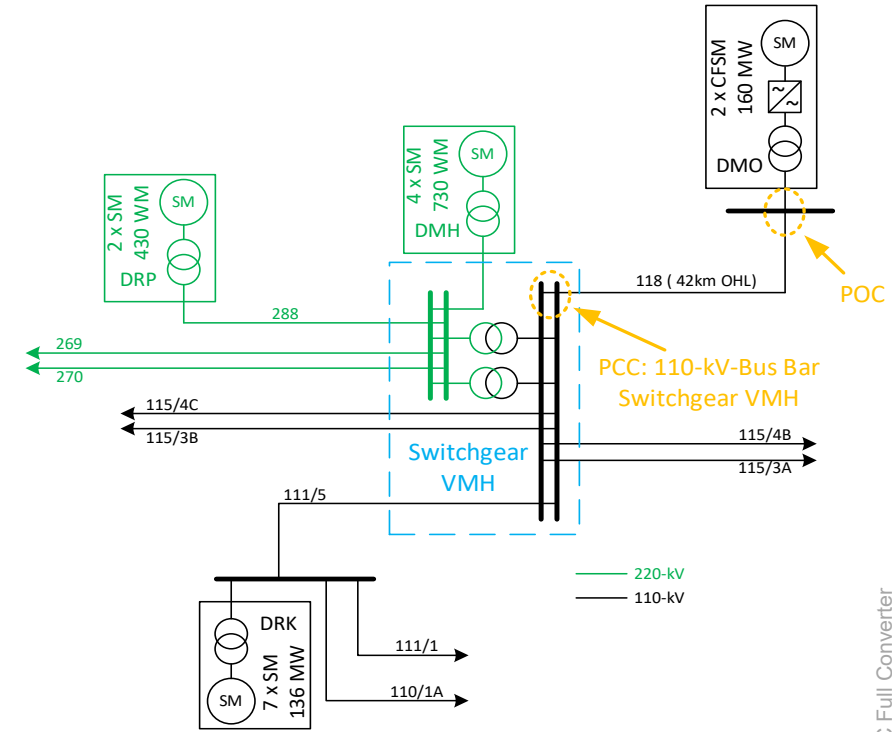
Harmonic Performance

Grid requirements

- Distortion level set by grid operator
- Half of the IEC 61000-3-6 planning level
- Relevant at PCC
- Harmonic studies during project phase
 - Measurements during commissioning

Measurement results

- Envelope of several operational points
- Worst Case considerations
 - No violations
- Little dependency on operational point
- Low order harmonics (< 20th) mainly from other sources
- System resonance around 43th
- Measurement confirms studies



Malfunction of winding fault protection

Problem

Winding fault protection false tripping

- Stator winding
- Transformer secondary windings

Evaluation of residual voltage at open D

- Voltage exceeds trigger level without fault
- Only in low power operation

Identified Cause

Caused by floating machine side

- Floating DC-Links oscillates close to fundamental
- Voltage transducer measure against grounding
- Oscillation occurs in measured residual voltage

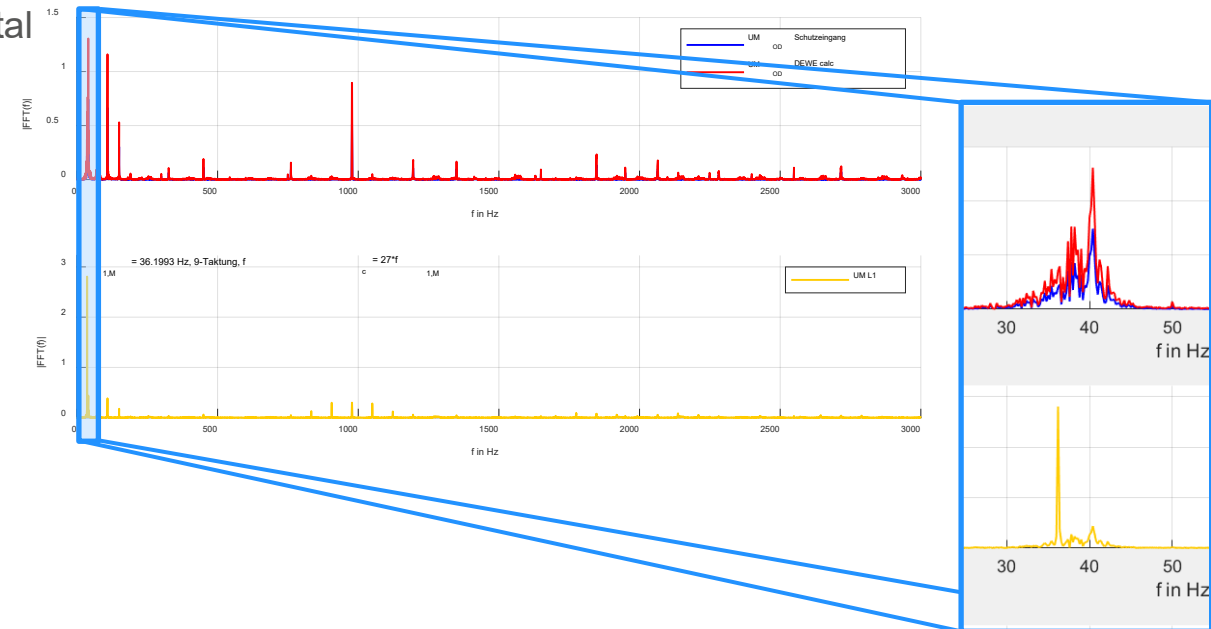
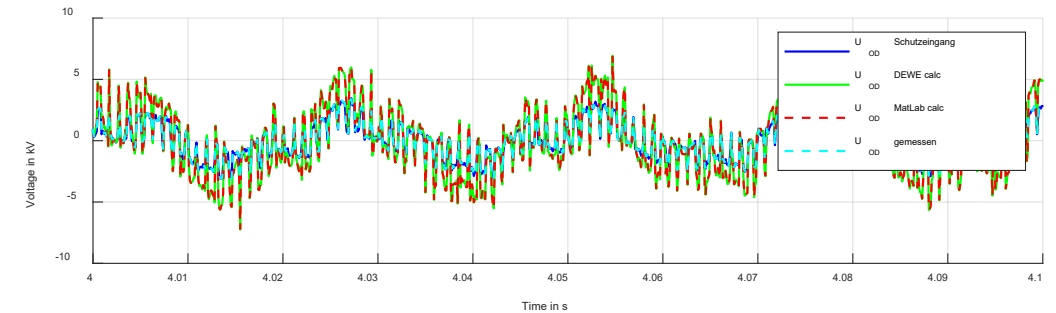
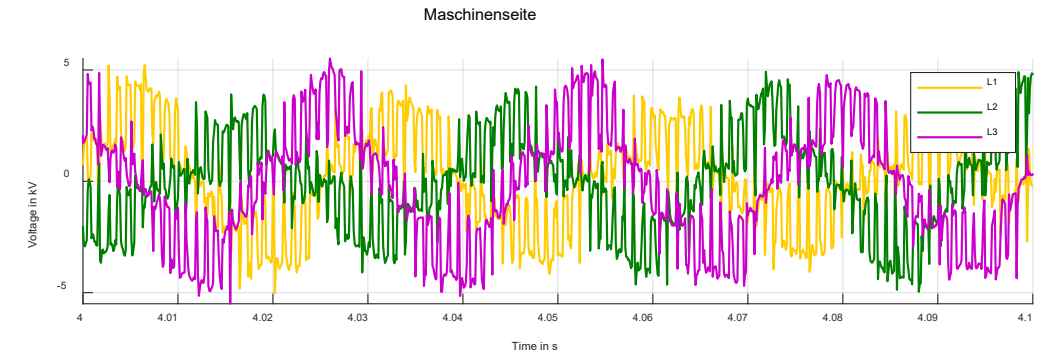
Remedy Action And Lessons Learned

Restriction of low speed operation

- Low power and low head
- Little operational influence

Active winding protection for future projects

- 20 Hz-method



High-frequency Shaft Voltage and bearing currents

Problem

Shaft voltages up to 700 V (peak – peak)

Risk of discharges at insulated bearing

- Bearing insulation
- Oil film

Discharges at sensors

Identified Cause

Common mode voltage Converter

- Caused by discrete output voltage
- Depends on pulsing pattern
- Capacitive coupling

Remedy Action And Lessons Learned

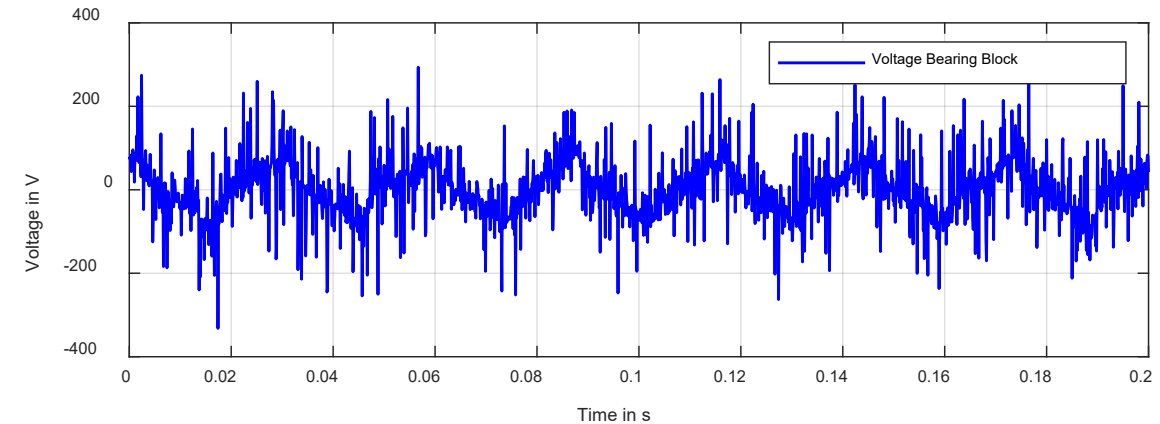
Short circuit path shaft to insulated bearing

- Protection of bearing surface

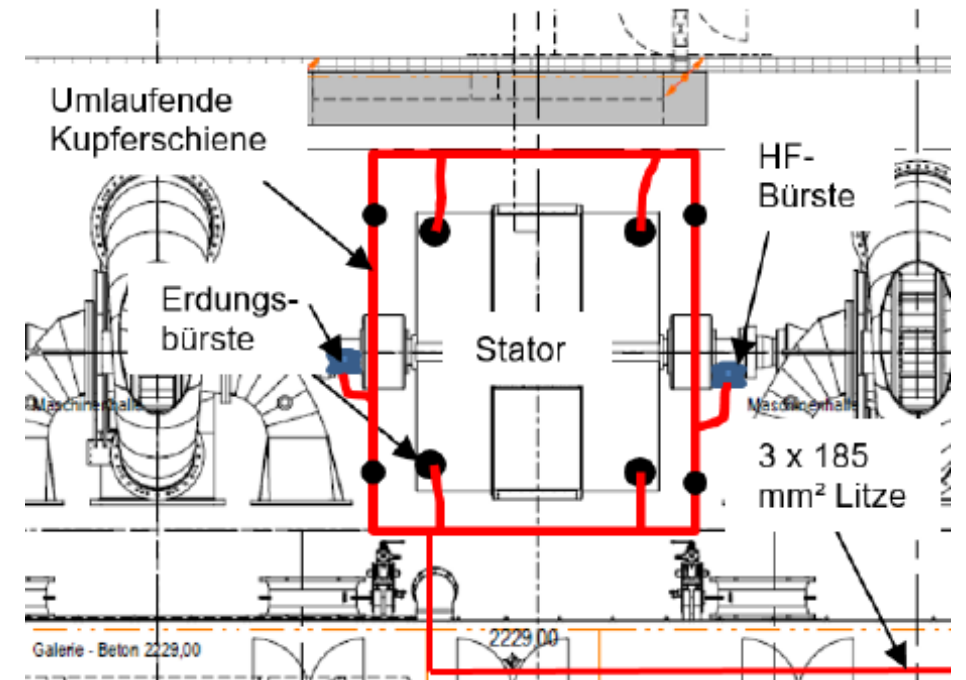
Additional high frequency grounding

- Reduction of shaft voltage
- RC configuration
- High impedance for low frequencies necessary

Low impedance grounding between generator and converter



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